

# New chiller development at Politecnico di Milano

**Marco Calderoni, Marco Guerra,  
Samuele Ambrosini**

Department of Energy, Politecnico di Milano  
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# Objectives of CASCO chiller

- Simplify chiller as much as possible (installation, maintenance)
- Avoid water based heat rejection
- Reduce auxiliary electricity consumption
- Simplify control strategy



The thermodynamic cycle is a dual lift water ammonia low temperature driven absorption cycle, in which the refrigerant flow self-adapts to the evaporator and absorber loads, making the system capable of adapting to variable loads and boundary conditions.

Thanks to self-adaptation capability, the chiller can well work without hot and cold storage, even at variable generator temperatures, which occur in solar assisted cooling.

A small storage can nevertheless be useful in order to provide the system with some inertia.

# RELAB: Polimi brand new test facility

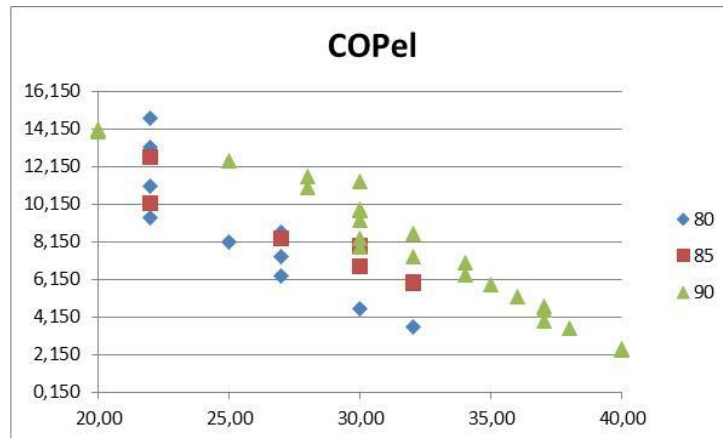
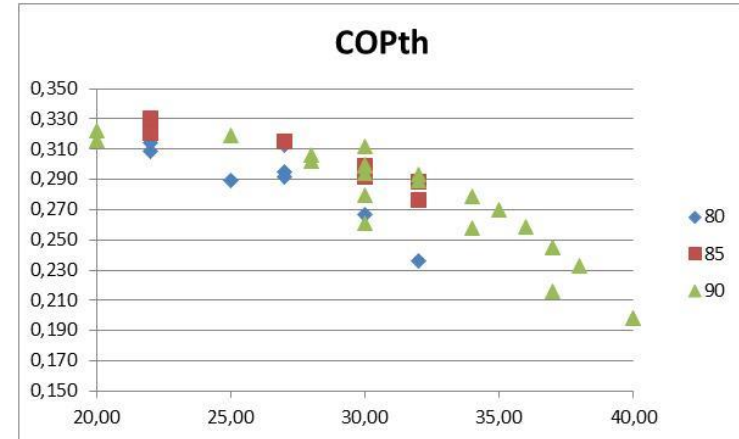
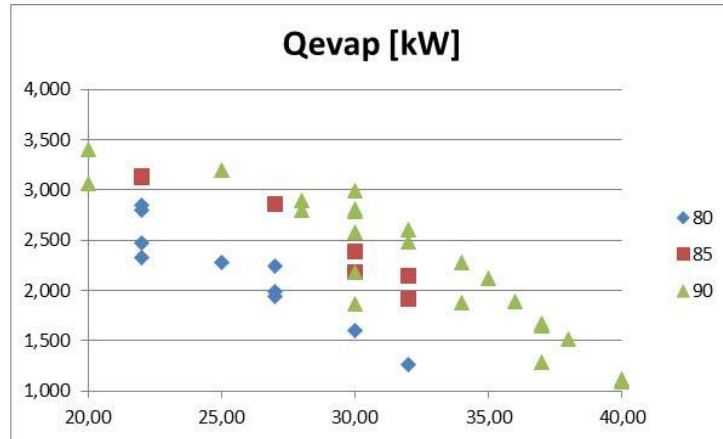
- One **Calibrated Calorimeter** for testing and developing appliances having nominal heating and cooling capacity up to **20 kW** :
  - *operative (accreditation EN 17025 expected by June 2014)*



- One **Climatic Chamber** for testing appliances having nominal heating and cooling capacity from **20kW to 100kW**:
  - *currently under construction*



# RELAB test lab results

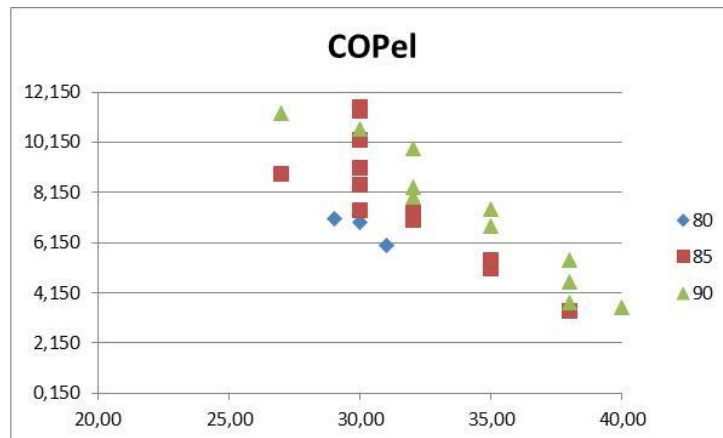
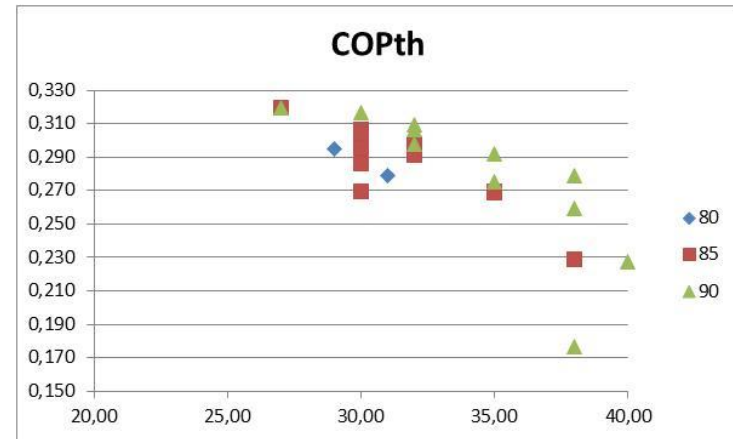
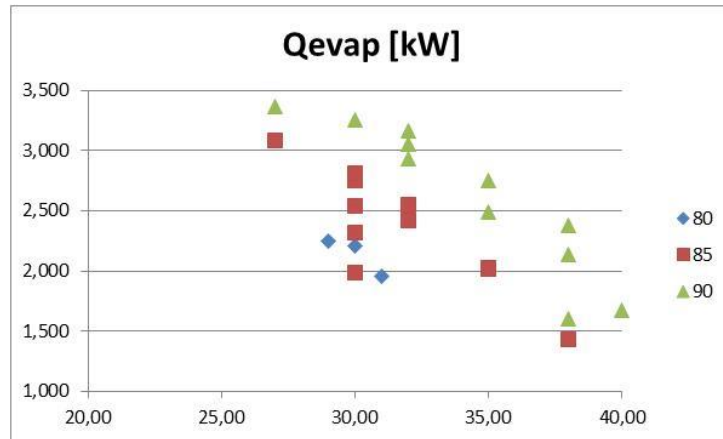


T evap= 7-12 °C

Delta T generator = 10 K

COP<sub>el</sub> includes electricity consumption of fan and solution pump.

# RELAB test lab results

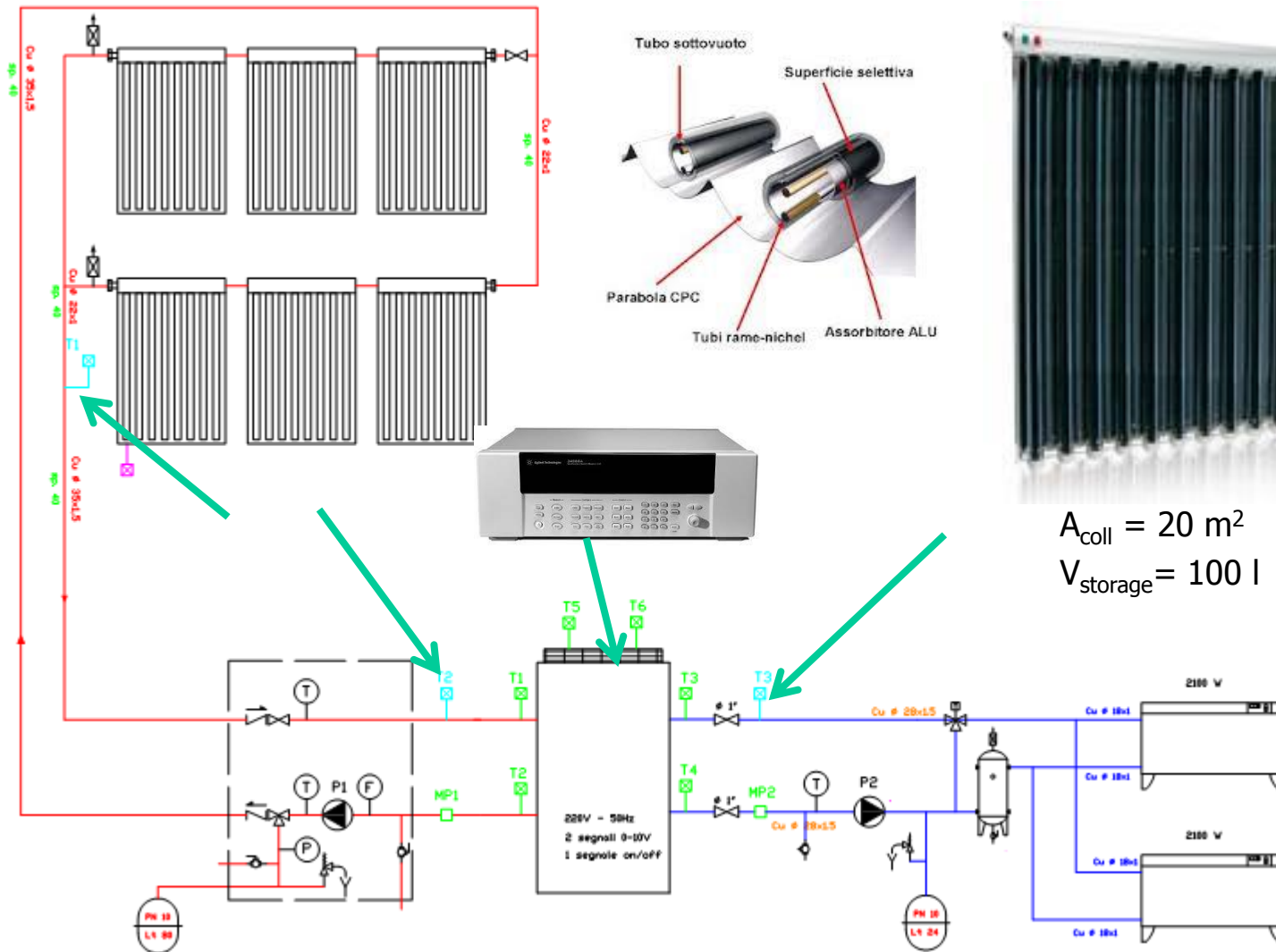


T evap= 7-12 °C

Delta T generator = 5 K

COP<sub>el</sub> includes electricity consumption of fan and solution pump.

# Outdoor testing



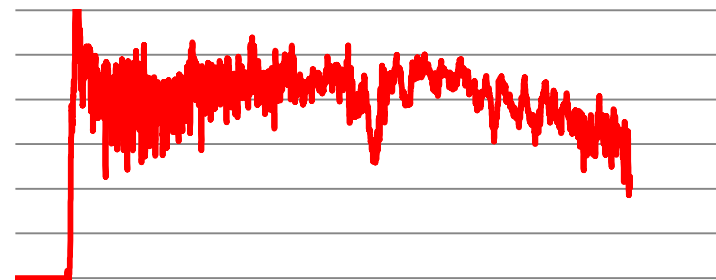
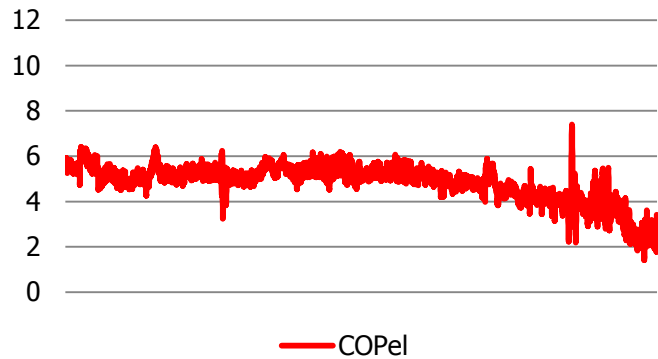
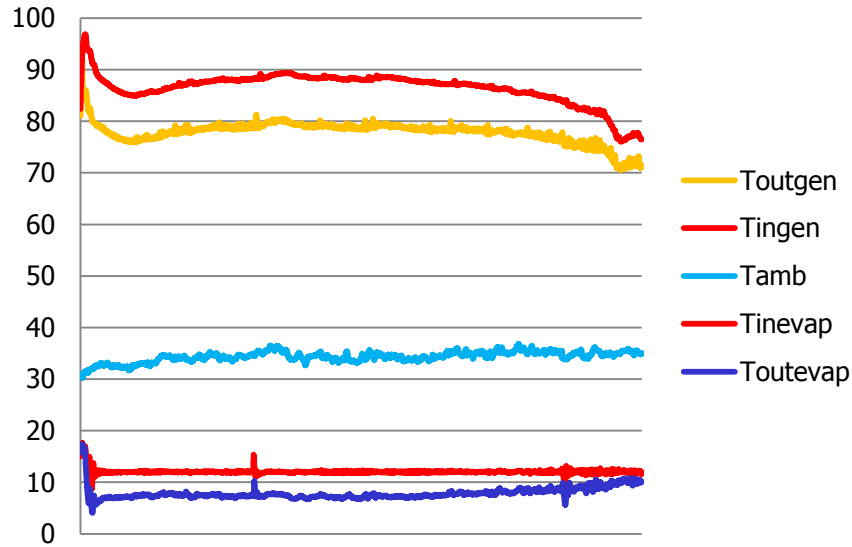
# Optimization of solar loop

A.  $m_{\dot{\text{sol}}} = 1.600 \text{ kg/h}$

- Pump consumption 125 W
- Increased average generator temperature
- Increased cooling power

B.  $m_{\dot{\text{sol}}} = 860 \text{ kg/h}$

- Pump consumption 35 W
- Decreased average generator temperature
- Decreased cooling power

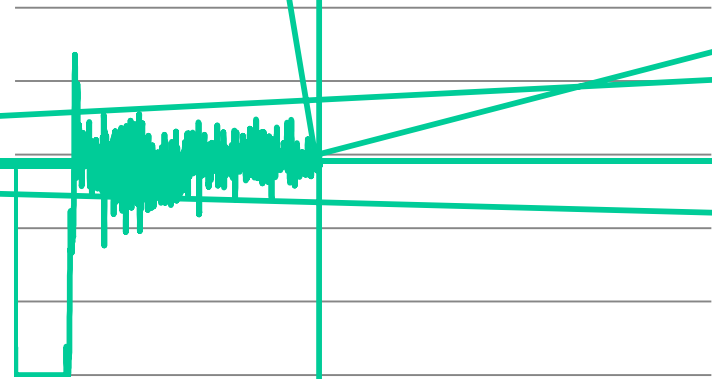




# Optimisation of fan control

Only  $T_{amb}$  available

$T_{amb}$  and  $T_{cond}$  available  $\rightarrow$   $\Delta T_{air}$  as control parameter



# First lab test results with negative temperatures

$T_{amb}$	$T_{gen}$	$T_{out,evap}$	$Q_{cold}$	$COP_{th}$	$COP_{el}$
°C	°C	°C	kW	-	-
25,01	90,23	-7,18	1,783	0,243	6,73
22,00	90,13	-10,84	1,782	0,247	8,87
14,99	90,11	-14,89	1,593	0,24	10,15

# Seasonal simulations with TRNSYS

$V_{\text{storage}}$	100 l	300 l
$\text{COP}_{\text{th}}$	0,306	0,297
$\text{COP}_{\text{el}}$	10,451	11,370
$Q_{\text{gen}}$ [kWh]	7199,73	8470,586
$Q_{\text{evap}}$ [kWh]	2351,80	2618,864
$Q_{\text{fan coil}}$ [kWh]	2281,11	2448,827
$I_{\text{coll}}$ [kWh/m <sup>2</sup> ]	977,25	977,249
$A_{\text{coll}}$ [m <sup>2</sup> ]	20	20
$\eta_{\text{coll}}$	36,8%	43,3%
$Q_{\text{el}}$ [kWh]	290,107	301,580
Operation time [h]	946,50	994,50
$\text{SCOP}_{\text{el}}$	7,85	8,12
% h discomfort	7,9%	2,68%
% comfort covered	80%	86%
$f_{\text{PE}}$	55%	60%

Comfort:  $T_{\text{in}} = 26^{\circ}\text{C}$

Discomfort:  $T_{\text{in}} > 27,5^{\circ}\text{C}$

Location	Milano
Type of building	residential
Building surface	102 m <sup>2</sup>
Cooling period	15/04-15/10
Peak demand	3,03 kW
Energy demand	2857 kWh/year

$$PE_{\text{sol}} = \frac{Q_{\text{backup}}}{\eta_{\text{boiler}} \cdot \varepsilon_{\text{fuel}}} +$$

$$PE_{\text{ref}} = \frac{Q_{\text{evap}}}{\text{SEER} \cdot \varepsilon_{\text{a}}}$$

$$SF_{\text{cool}} = 1 - \frac{Q_{\text{ba}}}{O}$$

$$f_{\text{PE}} = 1 - \frac{PE}{PE_{\text{ref}}}$$

$$\varepsilon_{\text{el,grid}} = 0,45 \quad \text{e} \quad \text{SEER} = 3,5$$

# Conclusions

- A solar cooling system for small residential applications has been installed on a virtual consumer, using a prototype of H<sub>2</sub>O/NH<sub>3</sub>, air cooled, half effect absorption chiller;
- Through monitoring activities fan and solar pump control have been optimized in order to reduce electricity consumption. By reducing unnecessary «overventilation» cooling power output decreases slightly, but electricity consumption is significantly reduced.
- Electrical performance is higher than most existing solar cooling plants, mainly due to little auxiliaries needed and control optimization;
- A performance map of the chiller has been developed;
- Simulations show that the system could cover approx. 85% of cooling demand of a domestic user, saving 60% of primary energy;
- Further optimization of the chiller:
  - Further increase heat exchangers performance by increasing  $HX_{\text{surface}}$  of better exploit available surface. Eventually experiment micro-channels HX.
- Further optimization of the system:
  - Build a solar cooling kit with commercial products (collectors, storage etc);
  - Optimize system's control.

## More information

- “Self adaptive refrigerant flow low temperature driven dual lift absorption cycle”, M. Guerra, 10th IIR Gustav Lorentzen Conference on Natural Refrigerants, Delft, The Netherlands, 2012
- [marco.calderoni@polimi.it](mailto:marco.calderoni@polimi.it)
- [marco.guerra@polimi.it](mailto:marco.guerra@polimi.it)

**Thank you for your attention!**

## Calibrated Calorimeter 20 kW Appliances that can be tested:

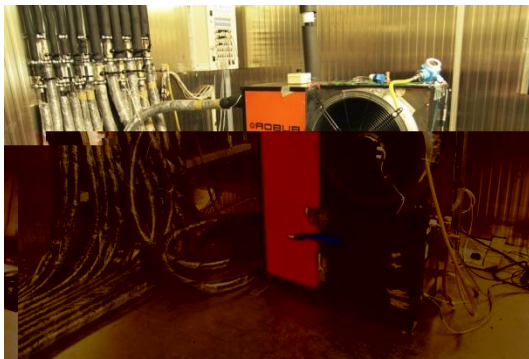
EN14511 & EN14825 - **Air Conditioners, Heat Pumps and Chillers** (*Air to Air – Air to Water– Water to Water (B/W) – Split & Packaged units*)

EN 16147 - **Heat Pumps for Domestic Hot water production**

EN 1397 - **Hydronic terminals** (*fan coils – dry coolers*)

EN 12309 - **Gas Fired heat pumps**

EN 308 - **Air and flue gases heat recovery devices** ( )



## Calibrated Calorimeter 20 kW

### Operating Ranges :

#### Outdoor Chamber

- Temperature range:  $-30\text{ °C} \div +60\text{ °C}$
- Relative Humidity Range:  $20\% \div 95\%$
- Temperature range in which the humidity is controlled:  $-16\text{ °C} \div +46$

#### Indoor Chamber

- Temperature range:  $+0\text{°C} \div +60\text{°C}$
- Relative Humidity Range:  $20\% \div 95\%$
- Temperature range in which the humidity is controlled:  $+5\text{°C} \div +46\text{°C}$

